

# Design of “model-friendly” turbulent non-premixed jet burners for C<sub>2+</sub> hydrocarbon fuels

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TABLE III. Flow parameters of the flames used in our experiments.

| Fuel | Re     | $Q^a$<br>(kW) | $Fr_f^b$ | $L_{f,e}^c$<br>(mm) | $L_{f,m}^d$<br>(mm) | $FR_f^e$<br>(slpm) | $FR_p^f$<br>(slpm) | $U^g$<br>(m/s) | $T_f^h$<br>(C) | $T_p^i$<br>(C) |
|------|--------|---------------|----------|---------------------|---------------------|--------------------|--------------------|----------------|----------------|----------------|
| C2H4 | 10 000 | 12.0          | 1.0      | 652                 | 730                 | 13.2               | 4.45               | 0.60           | 21             | 21             |
|      | 15 000 | 18.0          | 1.4      | 755                 | 775                 | 19.8               | 6.68               |                |                |                |
|      | 20 000 | 24.0          | 1.9      | 832                 | 830                 | 26.4               | 8.91               |                |                |                |
|      | 25 000 | 30.0          | 2.4      | 890                 | 861                 | 33.0               | 11.14              |                |                |                |
| JP-8 | 20 000 | 16.5          | 1.0      | 860                 | 872                 | 0.0295             | 6.09               | 0.67           | 300            | 205            |

<sup>a</sup>Heating value of the main fuel jet.

<sup>b</sup>Froude number of flame; for JP-8, assumes 40% radiation loss.

<sup>c</sup>Estimated visible flame length; for JP-8, assumes 40% radiation loss.

<sup>d</sup>Measured visible flame length.

<sup>e</sup>Volumetric flow rate of main fuel jet (liquid flow for JP-8).

<sup>f</sup>Volumetric flow rate of pilot flame premixture.

<sup>g</sup>Velocity of coflow air.

<sup>h</sup>Temperature of unburnt fuel.

<sup>i</sup>Temperature of pilot flame premixture.

2% of the heat release rate of the main fuel jet. Detailed flow parameters are listed in Table. Note that these flames with  $Fr_f$  ranging between 1.0 and 2.4 fall in the transitional regime, where both buoyancy and jet momentum are important. Predictable flame heights estimated from Eq. (1) generally match measured values well, confirming the validity of using this relation.

### III. PRELIMINARY CHARACTERIZATION

The open flame configuration permits convenient access for both optical and probe-based measurements. The primary comparison of these flames. Instead, we can compare the JP-8 canonical flames were characterized with qualitative methods to an ethylene flame established on the same (liquid-fuel), including direct photography, OH LIF planar imaging (fuel) burner with the same fuel jet (20 000). As shown in Fig. 8, these two flames look somewhat different. While the burner lip temperature boundary with line Rayleigh ethylene jet flame has a fairly long blue, soot-free region near the nozzle, the JP-8 flame is almost completely devoid of

learned from these preliminary measurements, such as the flame size, the frequency of occurrence of local extinction, and soot behavior.

#### A. Visual observation

In general, a sooty jet flame has a blue soot-free region near the nozzle (Fig. 1(c)) followed by a soot-laden region downstream. Soot produced in the flame is either consumed or escapes from the flame as smoke. The length of the soot-free region depends on the fuel, the fuel jet diameter, and the fuel jet velocity. Figure 7 presents fast-shutter photos of the four ethylene jet flames. With the 1/1600 s exposure time, the soot-free region is nearly invisible and the sooty regions appear orange, from the broad-band soot radiation. An increase in jet velocity pushes the sooty edge (the bottom edge of the soot-containing region) downstream. The photographs of the flames also show a progression in flame wrinkling with increasing  $Re$ . The flame with a Reynolds number of 10 000 shows smooth, large-scale vortex rollup, particularly as the distance from the nozzle increases (and buoyancy effects become relatively stronger). For flames with higher  $Re$ , the luminous flame front shows more intense wrinkling and smaller characteristic flame structures, reflecting a more turbulent flow field. The flame also broadens radially with the increase in  $Re$ , reflecting the increased rate of mixing between the fuel jet and the air coflow.

Since the JP-8 flame uses a burner with a smaller fuel jet diameter than the ethylene flames, there is limited value in comparing these flames. Instead, we can compare the JP-8 canonical flames were characterized with qualitative methods to an ethylene flame established on the same (liquid-fuel), including direct photography, OH LIF planar imaging (fuel) burner with the same fuel jet (20 000). As shown in Fig. 8, these two flames look somewhat different. While the burner lip temperature boundary with line Rayleigh ethylene jet flame has a fairly long blue, soot-free region near the nozzle, the JP-8 flame is almost completely devoid of



FIG. 10. (Color online) Instantaneous false-color OH PLIF images of three turbulent ethylene jet flames (a,  $Re = 15\,000$ ; b,  $Re = 20\,000$ ; c,  $Re = 25\,000$ ) and one JP-8 flame ( $Re = 20\,000$ ). The same intensity map was used to process all of the OH PLIF images.

local Rayleigh scattering cross section of the chemical species frequent local extinction followed by reignition downstream. mix in this region. Flames remain attached to the burner lip until the fuel jet

A similar measurement of the temperature boundary was increased beyond  $35\,000$ , when extinction becomes so severe that the flame is partially attached or lifted off from the sign of the pilot plate for this burner as for the gas burner burner. Clearly, this relationship between the flame Reynolds expected to give equivalent temperature profiles at the burner burner and extinction frequency is consistent with our prediction based on  $U_j/D$  as shown in Fig 2. It is also noted that, with the increase in  $Re$ , the OH layers at this height change from smooth sheets (Fig 10(a)) to rugged and kinked structures (Figs 10(b) and 10(c)), indicating the enhanced interactions between turbulence and the flame zone.

### C. OH LIF imaging

As OH is an important flame marker, planar imaging of OH is an effective method of capturing extinction events, which appear as breaks within otherwise continuous OH layers. To perform these measurements, a UV laser beam at  $283.55\text{ nm}$  was generated from the frequency doubled output of a YAG-pumped dye laser. The beam was shaped into a laser sheet with sheet-forming optics and subsequently intersected the flame on an axial plane, exciting OH radicals. The OH fluorescence was detected by an intensified CCD camera (ICCD-MAX, Princeton Instruments) operating with a  $100\text{ ns}$  exposure time using a  $105\text{-mm}$  focal length,  $f/4.5$  UV Nikkor lens and a band-pass filter set that transmits  $304\pm 320\text{ nm}$ . This OH detection scheme provides good discrimination against flame emission, laser scattering and fluorescence from polycyclic aromatics, but accepts fluorescence from single and double-ring aromatics.<sup>59</sup>

Figure 10 shows false-color OH LIF images centered about  $24$  jet diameters downstream, where strong strain coupled with diminishing influence of the pilot flame results in the highest probability of local flame extinction. For ethylene flames with a Reynolds number of  $15\,000$  or less, breakup of OH layers rarely occurs (Fig. 10(a)). Breaks in the OH layers are occasionally apparent in the ethylene flame with  $Re$  of  $20\,000$  (Fig. 10(b)), and become a frequent feature when the flame  $Re$  reaches  $25\,000$  and above (Fig. 10(c)), suggesting

Figure 10(d) shows an OH fluorescence image of the JP-8 flame over a similar range of near-burner heights as for the ethylene flame images. Note that the strong fluorescence around the jet axis ( $r/D = 0$ ) is due to small-ring aromatics,





